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**(54) THERMALLY ENHANCED COMPACT REFORMER**

**THERMISCH VERBESSERTE KOMPAKTE REFORMIERANLAGE**

**REFORMEUR COMPACT A RENFORCEMENT THERMIQUE**

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**(56) References cited:**

<b>EP-A- 0 330 751</b>	<b>EP-A- 0 572 017</b>
<b>WO-A-92/16029</b>	<b>WO-A-95/26430</b>
<b>WO-A-96/05625</b>	<b>GB-A- 2 057 908</b>
<b>GB-A- 2 210 286</b>	<b>US-A- 1 452 145</b>
<b>US-A- 2 127 561</b>	<b>US-A- 4 174 954</b>
<b>US-A- 4 770 955</b>	<b>US-A- 5 338 622</b>

- **PATENT ABSTRACTS OF JAPAN vol. 012, no. 011 (C-468), 13 January 1988 & JP 62 167203 A (HITACHI LTD), 23 July 1987,**
- **PATENT ABSTRACTS OF JAPAN vol. 014, no. 330 (C-0741), 16 July 1990 & JP 02 120206 A (YAMAHA MOTOR CO LTD), 8 May 1990,**
- **PATENT ABSTRACTS OF JAPAN vol. 016, no. 104 (E-1178), 13 March 1992 & JP 03 283266 A (NKK CORP), 13 December 1991, & JP 03 283266 A (NAKAGAWA HIROTAKA) 13 December 1991**
- **PATENT ABSTRACTS OF JAPAN vol. 012, no. 355 (E-661), 22 September 1988 & JP 63 110557 A (MITSUBISHI HEAVY IND LTD), 16 May 1988,**

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**EP 0 904 608 B1**

## Description

### Background of the invention

[0001] The present invention relates to reformers, and particularly to reforming apparatus that reforms fuel into fuel species suitable for use by electrochemical converters. In particular it relates to a plate type reformer suitable for either steam reforming or partial oxidation reforming.

[0002] The use of conventional hydrocarbon fuels as a fuel reactant for fuel cells is well known in the art. The hydrocarbon fuels are typically pre-processed and reformed into simpler reactants prior to introduction to the electrochemical converter. Conventionally, the fuel is pre-processed by passing the hydrocarbon fuel first through a desulfurization unit, then through a reformer, and a shift reactor (for H<sub>2</sub> fueled fuel cell only) to produce a suitable fuel stock.

[0003] Conventional steam reformers currently in wide commercial use comprise a reformer section consisting of a catalyst material which promotes the reforming reaction and a burner to supply heat for the endothermic reforming reaction. A steam source is typically connected to the reformer section to provide steam. The burner typically operates at temperatures well above that required by the reforming reaction and well above the operating temperatures of conventional fuel cells, e. g., solid oxide fuel cells. Because of this, the burner must be operated as a separate unit independent of the fuel cell and as such adds considerable bulk, weight, cost and complexity to the overall power system. Furthermore, the burner is not uniquely adaptable to utilize the waste heat generally available from the fuel cell. Moreover, the consumption of extra fuel by the burner limits the efficiency of the power system.

[0004] A typical tubular reformer contains multiple tubes, which are normally made of refractory metal alloys. Each tube contains a packed granular or pelletized material having a suitable reforming catalyst as a surface coating. The tube diameter typically varies from between 9 cm and 16 cm, and the heated length of the tube is normally between 6 and 12 meters. A combustion zone is provided external to the tubes, and is typically formed in the burner. The tube surface temperature is maintained by the burner in the range of 900°C to ensure that the hydrocarbon fuel flowing inside the tube is properly catalyzed with steam at a temperature between 500°C and 700°C. This traditional tube reformer relies upon conduction and convection heat transfer within the tube to distribute heat for reforming.

[0005] Plate-type reformers are known in the art, an example of which is shown and described in U.S. Patent No. 5,015,444 of Koga *et al.* The reformer described therein has alternating flat gap spaces for fuel/steam mixture flow and fuel/air mixture flow. The combustion of the fuel/air stream within the spaces provides the heat for reforming of the fuel/steam mixture stream. A draw-

back of this design is that the reformer relies upon heat transfer between the adjacent flat gap spaces to promote the fuel reforming process.

[0006] U.S. Patent No. 5,470,670 of Yasumoto *et al.* describes an integrated fuel cell/reformer structure, which has alternating layers of fuel cell and reformer plates. The heat transfer from the exothermic fuel cell to the endothermic reformer occurs through the thickness of the separating plates. A drawback of this design is that it is difficult to attain, if at all, temperature uniformities in this fuel cell/reformer structure, and which is essential in compact and efficient chemical or electrochemical apparatus designs. This fuel cell/reformer structure also requires complex and cumbersome reactant manifolding to interconnect the reactant flows between the alternating fuel cell layers and the reformer layers.

[0007] Electrochemical converters, such as fuel cells, have been known as systems for converting chemical energy derived from fuel stocks directly into electrical energy through electrochemical reaction. One type of fuel cell typically employed in fuel cell power generation systems is a solid oxide fuel cell. The solid oxide fuel cell generates electricity and releases waste heat at a temperature of about 1000°C.

[0008] A typical fuel cell consists mainly of a series of electrolyte units, onto which fuel and oxidizer electrodes are attached, and a similar series of interconnectors disposed between the electrolyte units to provide serial electrical connections. Electricity is generated between the electrodes across the electrolyte by an electrochemical reaction that is triggered when a fuel, e.g., hydrogen, is introduced at the fuel electrode and an oxidant, e.g., oxygen, is introduced at the oxidizer electrode.

[0009] Typically, the electrolyte is an ionic conductor having low ionic resistance thereby allowing the transport of an ionic species from one electrode-electrolyte interface to the opposite electrode-electrolyte interface under the operating conditions of the converter. The electrical current can be tapped for external load from the interconnector plates.

[0010] The conventional solid oxide fuel cell also includes, in addition to the features listed above, an electrolyte having a porous fuel and oxidizer electrode material applied on opposing sides of the electrolyte. The electrolyte is typically an oxygen ion conducting material, such as stabilized zirconia. The oxidizer electrode, which is typically maintained in an oxidizing atmosphere, is usually a perovskite of high electrical conductivity, such as strontium doped lanthanum manganite (LaMnO<sub>3</sub>(Sr)). The fuel electrode is typically maintained in a fuel rich or reducing atmosphere and is usually a cermet such as zirconia-nickel (ZrO<sub>2</sub>/Ni). The interconnector plate of the solid oxide fuel cell typically is made of an electronically conducting material which is stable in both an oxidizing and reducing atmosphere.

[0011] There still exists a need in the art for apparatus that utilizes the waste heat generated by the fuel cell for

reforming use. In particular, there exists a need for employing reformer design in close association with the electrochemical converters.

[0012] The invention will next be described in connection with certain preferred embodiments. However, it should be clear that various changes and modifications can be made by those skilled in the art without departing from the spirit and scope of the invention.

### Summary of the Invention

[0013] It is an object of the present invention to provide a plate-type reformer which has excellent thermal performance characteristics and allows effective thermal integration with a fuel cell. The invention further relates to a plate-type reformer which may be operated either as a steam reformer or as a partial oxidation reformer. When operating as a steam reformer it receives heat from a source such as a fuel cell, and receives steam from a source such as the exhaust of a fuel cell. The steam can be externally supplied from any conventional source, such as a steam boiler, or can be supplied by manifolding the exhaust of a conventional fuel cell to the reformer. The heat source can also be a combustion reactor. When operating as a partial oxidation reformer it combusts a relatively small portion, e.g., about 25%, of the incoming reactant gas to provide heat for the endothermic reforming reaction. The reformer is preferably capable of operating at an autothermal balanced condition which requires no other thermal input (heat source) nor steam supply. It is further capable of operating at a partial oxidation condition which is able to utilize the waste heat from a fuel cell.

[0014] Another object of the invention is to provide a plate-type reformer in which the catalyst is in intimate thermal contact with thermally conducting plates oriented, e.g., elongated, in the direction of the gas flow so that an average in-plane plate temperature is maintained to allow effective reforming reaction, as well as to eliminate or reduce the occurrence of hot spots which would be detrimental to the catalysts or structure materials of the reformer. The term "in-plane" is intended to mean the flat surfaces or side of the plate.

[0015] Still another object of the invention is to provide a plate-type reformer which is capable of utilizing the waste heat provided by the fuel cell for its endothermic reactions, either in steam reforming or in partial oxidation reforming.

[0016] Yet, another object of the invention is to provide a plate-type reformer which pre-heats the incoming reactants to a temperature suitable for reforming.

[0017] Another object of the invention is to provide a plate-type reformer in which multiple inlet manifolds are provided so that the reactants may be introduced to the reformer separately, and which are then thoroughly mixed within the reformer, before entering the oxidation section and the reformer section of the reformer.

[0018] In a first aspect, the invention provides a plate-

type reformer for reforming a reactant into reaction species during operation, said reformer being characterised in that it comprises a plurality of catalyst plates having associated therewith one or more catalyst materials for promoting reformation and a plurality of conductive plates formed of a thermally conducting material, said catalyst plates and said conductive plates being alternately stacked to form a reforming structure, the conductive plates conductively transferring heat energy in-plane to support the reforming process.

[0019] In a second aspect, the invention provides a reformer for reforming a reactant into a reaction species during operation, said reformer being characterised in that it includes:

a plurality of porous plates (38) formed of a composite of a thermally conductive material interspersed throughout the thickness of the plates with one or more catalyst materials for promoting the reforming process, said plates (38) being stacked together to form a reforming structure (10), the plates conductively transferring heat energy in-plane of the plates to support the reforming process.

[0020] In a third aspect, the invention provides a method for reforming a reactant into reaction species with a plate-type reformer (10), comprising the steps of

providing a plurality of catalyst plates (14) having associated therewith one or more catalyst materials for promoting reformation,

providing a plurality of conductive plates (12) formed of a thermally conducting material, stacking said catalyst plates (14) and said conductive plates (12) to form a plate-type reforming structure (10), and

conductively transferring heat energy in-plane across a surface (12A) of the conductive plate (12) to support the reforming process.

[0021] The reformer of the present invention employs a thermal enhancement feature which promotes efficient fuel reformation. According to one aspect, the reformer includes a planar catalyst configuration having interleaved thermally conducting plates. The latter feature greatly enhances the thermal characteristics of the reformer, resulting in a relatively compact reformer design. Hence, the reformer can be thermally and physically integrated with an electrochemical converter for efficiently reforming hydrocarbon fuel and generating electricity.

[0022] The invention overcomes the size disadvantages of conventional reformers by utilizing the foregoing efficient heat transfer techniques to achieve temperature uniformity (isothermal surfaces) and energy balance in the system. This temperature uniformity reduces the amount of reforming material necessary to reform the incoming reactants.

Furthermore, the thermal energy required by the endothermic reforming reactions is derived from the waste

heat of the thermally integrated electrochemical converter. For example, under normal operating conditions the converter generates excess or waste heat, which is used to support an operating temperature consistent with that required for reforming (in the range between about 500°C and about 700°C). Compactness and manifold simplicity are essential to provide a basis for economical reformer construction and system integration.

[0023] Other general and more specific objects of the invention will in part be obvious and will in part be evident from the drawings and description which follow.

### **Brief Description of the Drawings**

[0024] The foregoing and other objects, features and advantages of the invention will be apparent from the following description and apparent from the accompanying drawings, in which like reference characters refer to the same parts throughout the different views. The drawings illustrate principles of the invention and, although not to scale, show relative dimensions.

FIG. 1 is a cross-sectional view of one embodiment of an external fuel reformer according to the present invention;

FIGS. 2A-2C are cross-sectional views of various embodiments of the catalyst and reforming plates of FIG. 1.

FIG. 3 is an isometric view of an assembled electrochemical converter with internal reforming capability;

FIG. 4 is a more detailed isometric view of the electrolyte component and the interconnector component of an electrochemical converter allowing internal reforming;

FIG. 5 is a cross-sectional assembled view of the electrolyte component and interconnector component according to the invention illustrating the flow of reactants therethrough of external manifolding; and

FIG. 6 graphically illustrates that the interconnector plates provide the heat transfer function among the endothermic reforming strip and the exothermic combustion strip and the exothermic fuel cell strip, resulting in an isothermal in-plane temperature.

### **Description of Illustrated Embodiments**

[0025] FIG. 1 is a cross-sectional view of the reformer 10 of the present invention. The reformer 10 includes a number of thermally conductive plates 12 and reforming plates 14 that are alternately stacked together to form a stacked reforming structure 13 that extends along axis 28. The reformer includes a fluid conduit 16 that is in fluid communication with the inner portions 12A, 14A of the plates 12, 14. The reformer 10 is preferably housed within a gas-tight enclosure or housing 20. The illustrat-

ed reformer can be used to perform both steam and oxidation reforming. The heat necessary for the reforming process can be supplied internally by partial oxidation of hydrocarbon fuel or supplied externally by a remote heat source, as shown by wavy lines 26, to the reformer 10 by radiation, conduction or convection.

[0026] The reactant to be reformed by the reformer 10 is introduced into the apparatus through the axial fluid manifold 16. The reactant preferably comprises a mixture of a hydrocarbon fuel and a reforming agent, such as air, oxygen, water or CO<sub>2</sub>, that are premixed either prior to introduction to the manifold 16 or within the reformer. The illustrated reformer 10 includes at least one manifold that delivers a fuel/reforming agent mixture to the reformer, rather than provide separate input manifolds for each gas constituent. The introduction of a premixed reactants to the reformer 10 provides for a relatively simple design.

[0027] The reactant mixture 22 is introduced to the manifold 16 by any appropriate means, such as by fluid conduits. The mixture 22 enters the inner portions of the reformer through reactant passages 24 that are formed between the adjacent conductive plates 12 and reforming plates 14. The passages can comprise any surface indentation or protrusions, which can be formed by embossing, and which constitutes a substantially continuous fluid passage that extends from the manifold 16 to the outer peripheral surface 13A of the stacked reforming structure 13. The passages can also be formed by utilizing conductive or reforming plates that are made of a porous material or have a power reformer catalyst material coated or formed thereon, thus allowing the reactant to pass through the reformer.

[0028] Examples of these various plate arrangements and configurations are illustrated in FIGS. 2A-2C. FIG. 2A illustrates the stacked arrangement of the reformer plates 14 and conductive plates 12. The reformer plates preferably have formed thereon a reformer catalyst material 36 that intimately contacts the conductive plate 12. The illustrated conductive plate 12 is embossed to form reactant flow channels. The mixture 22 is introduced to the axial manifold 16 and enters the reactant channels, where it exits the stacked plate reformer at the peripheral edges thereof.

[0029] The reformer catalyst material can be composed of a solid or porous material. FIG. 2B illustrates the mixture flow through the reformer 10 when using a porous reforming material. The use of a porous reforming material relaxes the embossing requirements of the illustrated reformer.

[0030] In another embodiment, as illustrated in FIG. 2C, the reformer 10 includes a plurality of stacked plates 38 or simply a columnal structure that are formed of a composite of thermally conductive material and a reforming material. This composite plate 38 can be achieved by interspersing a suitably thermally conductive material in admixture with a suitable reforming material. The resultant stacked structure operates substan-

tially identical to the stacked reforming structure 13 shown in FIGS. 1, 2A and 2B and described above.

[0031] Those of ordinary skill will recognize that other embodiments of the reformer 10 exists, such as where the reforming plates 14 are composed of a porous material and have a reforming catalyst material disposed therein or coated thereon. The use of porous materials is one of the advantages of the present external reformer since it relaxes the gas-tight requirements of the reforming system without sacrificing efficiency.

[0032] The reactant mixture is reformed within the stacked reforming structure 10 as the reactant passes through the reactant passages and over or through the reforming plates 14. The catalyst material associated with the reforming plates 14 promotes the reforming of the hydrocarbon fuel into simpler reaction species. The stream of reactant mixture introduced to the manifold 16 can comprise  $H_2O$ ,  $O_2$ , and  $CO_2$ , in addition to a hydrocarbon fuel. For example, methane ( $CH_4$ ) can be catalytically reformed into a mixture of hydrogen, water, carbon monoxide and carbon dioxide.

[0033] When operating the reformer as a steam reformer, it receives a reactant gas mixture containing natural gas (or methane) and steam. Steam reforming catalyst can be formed on the reformer plate in a circumferential band. Thermal energy for the reforming reaction is preferably conducted radially inward from the gas-tight enclosure by the conductive plates 12. The thickness and thermal conductivity of the conductive plates are selected to provide sufficient heat flow radially (or in-plane) to provide heat for the endothermic reforming reaction. The conductive plate can include an integral extension which protrudes into the axial reactant manifold 16 for preheating the incoming reactants, as described in further detail below.

[0034] When operating the reformer as a partial oxidation reformer, it receives a reactant gas mixture containing natural gas (or methane) and air or oxygen. One or more types of reforming catalyst material can be distributed in circumferential bands on the reformer plate. According to one aspect, the plate can include an inner band which contains a combustion catalyst 92, and a radially outer band 90 which contains catalyst to promote reforming of methane by water vapor (steam reforming) and by carbon dioxide. Thermal energy for these endothermic reforming reactions is conducted radially from the combustion band to the reforming band by the plate 12. Catalysts for other reactions, such as conventional shift reactions that convert CO in the presence of  $H_2O$  to form  $H_2$  and  $CO_2$  may also be incorporated. The thickness and thermal conductivity of the conductive plates 12 are selected to provide sufficient heat flow radially between the inner combustion band and the outer reforming band to supply heat energy for the endothermic reforming reactions. The conductive plates 12 also provide sufficient heat flow radially from the combustion band to pre-heat the incoming reactants at the inlet passages 24 to near operational tempera-

tures, e.g., at least about  $300^\circ C$ . The thermal energy of the system is preferably transferred from the external source to the reformer 10 through the gas-tight enclosure 20.

[0035] The illustrated reformer 10 can be used to reform reactants such as alkanes (paraffin hydrocarbons), hydrocarbons bonded with alcohols (hydroxyls), hydrocarbons bonded with carboxyls, hydrocarbons bonded with carbonyls, hydrocarbons bonded with alkenes (olefins hydrocarbons), hydrocarbons bonded with ethers, hydrocarbons bonded with esterhydrocarbons bonded with amines, hydrocarbons bonded with aromatic derivatives, and hydrocarbons bonded other organo-derivatives.

[0036] The band of reforming material of the reformer 10 can be located and mixed in varying proportions to maximize the production of reformed gas.

[0037] The reforming plate 14 can be composed of any suitable reforming catalytic material that operates at temperatures in the range between about  $200^\circ C$  and about  $800^\circ C$ . Examples of the types of material that can be used include platinum, palladium, chromium, chromium oxide, nickel, nickel oxide, nickel containing compounds, and other suitable transition metals and their oxides. The reforming plate 14 can further include a ceramic support plate that has a reforming material coated thereon, as illustrated in FIGS. 2A and 2B. Thus, the reforming plate 14 of the present invention can include any multi-stacked reforming plate structure that includes suitable reforming catalysts that promote the reformation of a hydrocarbon fuel into suitable reaction species.

[0038] The conductive plate 12 can be formed of any suitable thermally conductive material, including metals such as aluminum, copper, iron, steel alloys, nickel, nickel alloys, chromium, chromium alloys, platinum, and nonmetals such as silicon carbide, and other composite materials. The thickness of the conductive plate 12 can be selected to maintain a minimum temperature gradient in-plane of the plate 12 and to thereby provide an isothermal region for optimum reforming reaction and to alleviate thermal stress in the reforming plates 14. The conductive plate 12 preferably forms a near isothermal condition in-plane of each plate 12. The isothermal surface formed by the conductive plate 12 improves the efficiency of the overall reforming process by providing a substantially uniform temperature and supply of heat over the surface of the plate for reforming.

[0039] Furthermore, the conductive plates form an isothermal condition along the axis of the stack (along the outer peripheral surface of the stacked reformer 13) by the uniform distribution of the reactant mixture through the reactant passages, thereby preventing cold or hot spots from developing along the stack. This improves the thermal characteristics of the reformer 10 and improves the overall performance of the system. As used herein, the term "isothermal" condition or region is intended to include a substantially constant temperature that varies only slightly in an axial or in-plane direction.

A temperature variation of about 50°C is contemplated by the teachings of the present invention.

[0040] The reformed fuel or reaction species is exhausted along the peripheral portion 13A of the stacked reforming structure 13, as indicated by wavy lines 30. The peripheral exhausting of the reaction species, e.g., reformed fuel products allows relatively easy manifolding of the reactants. The exhausted fluid media are then collected by the gas-tight housing 20 and exhausted therefrom through exit conduits 32. The gas-tight housing 20 thus serves as a peripheral manifold.

[0041] In an alternate embodiment, the reactant mixture 22 can be introduced into the peripheral manifold formed by the housing 20 and then into the stacked reforming structure 13 along the peripheral edge. The reactant flows radially inward across the reforming and conductive plates 14, 12 and is discharged through the axial manifold 16.

[0042] The ability to vent the reformed reactant mixture at least at a substantial portion of the periphery of the stack, and preferably from nearly the entire periphery, provides for an exposed peripheral surface devoid of a gas-tight seal or insulating material. Hence, the external reformer 10 of the present invention achieves a compact, simple, elegant external reforming design.

[0043] The gas-tight enclosure 20 is preferably composed of a thermally conductive material, such as metal. In the illustrated embodiment, the gas-tight enclosure 20 radiantly receives heat energy from an external heat source and further radiantly transfers this heat energy to the stack 13 and thus to the conductive plates 12. The plates 12 supply the heat energy necessary for the reforming reaction by conductively transferring the heat from the outer peripheral surface 13A of the stack 13 inwardly towards the reactant manifold 16.

[0044] In another embodiment, the outer surface of the reforming structure 10 contacts the inner surface of the gas-tight housing, which serves to conductively transfer the heat energy to the conductive plates.

[0045] The gas-tight enclosure of cylindrical configuration is particularly suitable for pressurized reformer operation. The pressure within the vessel is preferably between about ambient and about 50 atm.

[0046] The technique for achieving axial reactant flow distribution uniformity is as follows. The reactant flow passages 24 are designed to ensure that the total reactant flow pressure drop in the reactant passages is significantly greater than or dominates the reactant flow pressure drop in the reactant manifold 16. More specifically, the flow resistance of the passages 24 is substantially greater than the flow resistance of the axial manifold 16. According to a preferred practice, the reactant flow pressure within the passages 24 is about ten times greater than the reactant flow pressure within the manifold. This pressure differential ensures an axial and azimuthal uniform distribution of reactant along the reactant manifold 16 and the reactant passages 24 and essentially from top to bottom of the reformer stack 13. The

uniform flow distribution ensures a uniform temperature condition along the axis of the reforming structure 10.

[0047] According to a preferred embodiment, the stacked reforming structure 13 is a columnal structure, and the plates have a diameter between about 1 inch and about 20 inches, and has a thickness between about 0.002 inch and about 0.2 inch. The term columnal as used herein is intended to describe various geometric structures that are stacked along a longitudinal axis and have at least one internal reactant manifold which serves as a conduit for a reactant mixture.

[0048] Those of ordinary skill will appreciate that other geometric configurations can be used, such as rectangular or rectilinear shapes with internal or external manifolds. The plates having a rectangular configuration can be stacked and integrated with attached external manifolds for the supply and the collection of the reactant and reforming resultant species.

[0049] The relatively small dimensions of the plates 12, 14 of the reformer 10 provide for a compact plate-type reformer that reforms a hydrocarbon fuel into suitable reaction species, and which is easily integratable with existing power systems and assemblies. The illustrated reformer 10 can be thermally integrated with an electrochemical converter, such as a solid oxide fuel cell. In the special application where the reformed fuel is introduced into the fuel cell, the required heat of reaction is supplied from the waste heat generated by the fuel cell.

[0050] According to another practice of the present invention, the reformer structure of Figure 1 can also function as a plate-type burner. Specifically, hydrocarbon fuel can be oxidized in the presence of air or other oxidants with or without a suitable catalyst material. The burner embodiment of the present invention includes a conductive plate 12 and a catalyst plate 14 that are alternately stacked together, as described above in relation to the reformer of Figure 1. The burner can employ an input manifold 16 to introduce the incoming reactant to the burner. The incoming reactants can comprise a hydrocarbon fuel and an oxidant, such as air. The hydrocarbon fuel and oxidant can be separately manifolded to the burner or can be premixed. For example, if substantially gas-tight materials are used to form the plates 12, 14, the reactants are premixed either prior to introduction to the burner or within the input manifold. Conversely, if either plate is formed of a porous material, the reactants can be separately manifolded. The reactants passing across the porous material of the plate then pass therethrough and mix with the other reactant within the reactant passages. The combusted or oxidized reactant is then discharged about the periphery of the burner stack. The oxidized reactant or the resultant species includes CO<sub>2</sub>, H<sub>2</sub>O and other stable combustion products depending upon the type of fuel.

[0051] The conductive plate of the burner is identical to that of the reformer and functions to conductively transfer heat in-plane of the plate to form an isothermal

surface. The thickness of the conductive plate is designed to maintain a minimum temperature gradient in-plane of the plate to provide an isothermal region for optimum combustion reaction to produce reduced NO<sub>x</sub>, if air is used as the oxidant, and to alleviate thermal stress in the catalyst plates 14.

[0052] Furthermore, the isothermal condition can be maintained by the uniform distribution of reactants of along the axis of the stack, thus preventing cold hot spots from developing along the stack. This improves the overall thermal characteristics of the burner and improves the overall operating performance of the burner.

[0053] The illustrated burner further includes reactant flow passages 24, as set forth above in conjunction with the reformer 10. The reactant passages 24 are designed to ensure that the total reactant flow pressure drop in the reactant passages 24 is significantly greater than the reactant flow pressure drop in the reactant manifold 16. More specifically, the flow resistance the passages 24 is substantially greater than the flow resistance in the axial manifold 16. This pressure differential ensures an axial and azimuthal uniform distribution of reactant throughout the axial length of the burner.

[0054] The oxidized reactant can be discharged about the peripheral portion of the burner. The exhausted fluid mediums can be captured by a gas-tight housing 20 that surrounds the burner.

[0055] In an alternate embodiment, the burner can include a plurality of stacked plates that are formed of a composite of a thermally conductive material and a catalyst material. This composite plate can be achieved by interspersing a suitably thermally conductive material in admixture with a suitable catalytic material. The resulting stacked structure operates substantially identical to the stacked reforming structure 13 shown in Figure 1 and described above.

[0056] In an alternate embodiment, the burner can include a cylindrical column that is formed of a composite of a thermally conductive material and a catalyst material by interspersing a suitably thermally conductive material in admixture with a suitable catalytic material. The resulting reforming structure operates substantially identical to the stacked reforming structure 13 shown in Figure 1 and described above.

[0057] All other features discussed above in relation to the reformer are equally applicable to the burner.

[0058] FIG. 3 shows an isometric view of a reformer incorporated internal to an electrochemical converter according to a preferred embodiment of the invention. The internal reforming electrochemical converter 40 is shown consisting of alternating layers of an electrolyte plate 50 and an interconnector plate 60. The interconnector plate is typically a good thermal and electrical conductor. Holes or manifolds formed in the structure provide conduits for the fuel and oxidizer gases, e.g., input reactants. Reactant flow passageways formed in the interconnector plates, FIG. 4, facilitate the distribution and collection of these gases.

[0059] The plates 50, 60 of the internal reforming electrochemical converter 40 are held in compression by a spring loaded tie-rod assembly 42. The tie-rod assembly 42 includes a tie-rod member 44 seated within a central oxidizer manifold 47, as shown in FIG. 4, that includes an assembly nut 44A. A pair of endplates 46 mounted at either end of the internal reforming electrochemical converter 40 provides uniform clamping action on stack of alternating interconnector and electrolyte plates 50, 60 and maintains the electrical contact between the plates and provides gas sealing at appropriate places within the assembly.

[0060] FIGS. 3 through 5 illustrate the basic cell unit of the electrochemical converter 40, which includes the electrolyte plate 50 and the interconnector plate 60. In one embodiment, the electrolyte plate 50 can be made of a ceramic material, such as a stabilized zirconia material  $ZrO_2(Y_2O_3)$ , an oxygen ion conductor, and a porous oxidizer electrode material 50A and a porous fuel electrode material 50B which are disposed thereon. Exemplary materials for the oxidizer electrode material are perovskite materials, such as  $LaMnO_3(Sr)$ . Exemplary materials for the fuel electrode material are cermets such as  $ZrO_2/Ni$  and  $ZrO_2/NiO$ .

[0061] The interconnector plate 60 preferably is made of an electrically and thermally conductive interconnect material. The materials suitable for interconnector fabrication include metals such as aluminum, copper, iron, steel alloys, nickel, nickel alloys, chromium, chromium alloys, platinum, platinum alloys, and nonmetals such as silicon carbide,  $La(Mn)CrO_3$ , and other electrically conductive materials. The interconnector plate 60 serves as the electric connector between adjacent electrolyte plates and as a partition between the fuel and oxidizer reactants. Additionally, the interconnector plate 60 conductively transfers heat in-plane (e.g., across the surface) of the plate to form an isothermal surface, as described in further detail below. As best shown in FIG. 4, the interconnector plate 60 has a central aperture 62 and a set of intermediate, concentric radially outwardly spaced apertures 64. A third outer set of apertures 66 are disposed along the outer cylindrical portion or periphery of the plate 60.

[0062] The interconnector plate 60 can have a textured surface. The textured surface 60A preferably has formed thereon a series of dimples, which are formed by known embossing techniques and which form a series of connecting reactant flow passageways. Preferably, both sides of the interconnector plate have the dimpled surface formed thereon. Although the intermediate and outer set of apertures 64 and 66, respectively, are shown with a selected number of apertures, those of ordinary skill will recognize that any number of apertures or distribution patterns can be employed, depending upon the system and reactant flow and manifolding requirements.

[0063] Likewise, the electrolyte plate 50 has a central aperture 52, and a set of intermediate and outer aper-



tures 54 and 56 that are formed at locations complementary to the apertures 62, 64 and 66, respectively, of the interconnector plate 60.

[0064] As shown in FIG. 4, a reactant flow adjustment element 80 can be interposed between the electrolyte plate 50 and the interconnector plate 60. The flow adjustment element 80 serves as a fluid-flow impedance between the plates 50, 60, which restricts the flow of the reactants in the reactant flow passageways. Thus, the flow adjustment element 80 provides for greater uniformity of flow. A preferred flow adjustment element is a wire mesh or screen, but any suitable design can be used provided it serves to restrict the flow of the reactants at a selected and determinable rate.

[0065] Referring to FIG. 4, the electrolyte plates 50 and the interconnector plates 60 are alternately stacked and aligned along their respective apertures. The apertures form axial (with respect to the stack) manifolds that feed the cell unit with the input reactants, and that exhaust spent fuel. In particular, the central apertures 52, 62 form input oxidizer manifold 47, the concentric apertures 54, 64 form input fuel manifold 48, and the aligned outer apertures 56, 66 form spent fuel manifold 49.

[0066] The absence of a ridge or other raised structure at portion of the periphery of the interconnector plate provides for exhaust ports that communicate with the external environment. The reactant flow passageways connect, fluidwise, the input reactant manifolds 47 and 48 with the outer periphery of the reformer 40, thus allowing the reactants to be exhausted externally of the converter.

[0067] The internal reforming electrochemical converter is a stacked plate assembly of cylindrical configuration, and at least one of the electrolyte plate and the conductive plate has a diameter between about 1 inches and about 20 inches, and has a thickness between about 0.002 inches and about 0.2 inches.

[0068] The internal reforming electrochemical converter 40 of this invention has incorporated therein additional features as described below. The internal reforming operation when performed in the presence of steam receives a reactant gas mixture containing natural gas (or methane) and steam. A steam reforming catalyst 90, (FIG. 5) is distributed in a circumferential band that precedes the fuel electrode material 50B on the electrolyte plate 50. Thermal energy for the reforming reaction is conducted radially by the plate 60 to the reforming band. The thickness and thermal conductivity of the plates is designed to provide sufficient heat flow radially between the inner reforming band 90 and the outer fuel cell band (e.g., band 50B) to provide heat energy for the endothermic reforming reaction and to pre-heat the incoming reactants.

[0069] The internal reforming can also be performed by a partial oxidation reaction. In this mode, the illustrated converter 40 receives a reactant gas mixture containing natural gas (or methane) and air or oxygen. One or more types of catalyst are distributed in circumferen-

tial bands preceding the fuel electrode 50B on the electrolyte plate 50. As shown in FIG. 5, the electrolyte plate includes an inner band that contains a combustion catalyst 92, a radially outer band 90 that contains catalysts to promote reforming of methane by water vapor (steam reforming) and by carbon dioxide. Thermal energy for these endothermic reforming reactions is conducted radially from the combustion band 92 to the reforming band 90. Catalysts for other reactions, e.g. shift reactions etc. may also be incorporated. The thickness and thermal conductivity of the conductive plates is designed to provide sufficient heat flow radially between the inner combustion band 90 and the radially outer reforming band 90 to provide the endothermic reaction energy and to pre-heat the incoming reactants. Additional thermal energy can be obtained from the exothermal fuel cell reaction performed by the fuel electrode 50B illustrated as an outermost band along the diameter of the plate.

[0070] In the illustrated electrochemical converter 40, the combustion catalyst 92, the reforming catalyst 90 and a shift catalyst (which can be also applied as a band radially outward of the reforming catalyst 80) can also be applied on the flow adjustment element, which is situated between the electrolyte plate and the conductive plate.

[0071] The reformer may apply the catalysts which are mixed in varying proportions radially to maximize the production of product gas.

[0072] All of the reforming features discussed above in relation to the external reformer and band are equally applicable to this internal reforming electrochemical converter. For example, the interconnector plate 60 can include extended lip portions 72A and 72B, either of which can be used to preheat incoming reactants.

[0073] The internal reforming electrochemical converter 40 of the present invention can be a fuel cell, such as a solid oxide fuel cell, molten carbonate fuel cell, alkaline fuel cell, phosphoric acid fuel cell, and proton membrane fuel cell. The preferred fuel cell of the present invention is a solid oxide fuel cell. The internal reforming electrochemical converter 40 of the present invention preferable has an operating temperature above 600°C, and preferably between about 900°C and 1100°C, and most preferably about 1000°C.

[0074] Those of ordinary skill will appreciate that the illustrated combustion, reforming and fuel electrode bands are merely representative of relative locations of electrochemical operations that occur during use of the converter 40 as a reformer.

[0075] In another embodiment of the invention, the internal reforming electrochemical converter 40 can have any desirable geometric configuration, such as a rectangular configuration. The stacked structure can thus include rectangular electrolyte plates 50 and rectangular interconnector plates 60 with manifolds attached external to the plates. The catalytic and electrode materials can be applied in strips on the electrolyte plates perpen-

dicular to the reactants flow direction. As illustrated in FIG. 5, the fuel flow 24 is perpendicular to the elongated bands 92, 90 and 50B. The interconnector plates 60 conductively transfer heat energy to the endothermic reforming catalyst band 90, the exothermic combustion catalyst band 92, and the exothermic fuel cell band 50B, resulting in a substantially in-plane isothermal condition, as illustrated in FIG. 6.

[0076] FIG. 6 graphically depicts the isothermal temperature condition of the incoming reactants, e.g., hydrocarbon fuel, and reformed fuel established by the thermally conductive plate 60 during its passages over the electrolyte plate 50. The temperature of the fuel during operation is defined by the ordinate axis and the fuel flow direction is defined by the abscissa. In a reforming structure that does not utilize a thermally conductive plate to transfer heat in-plane during operation, the fuel temperature varies greatly in the direction of fuel flow, as denoted by waveform 110. As illustrated, the incoming fuel is initially preheated, as by the extended surfaces 72A and 72B. This preheating stage 112 corresponds to a rise in the fuel temperature as it approaches the operating temperature of the converter 40. During the exothermic partial oxidation or combustion stage 114, the temperature of the fuel further increases until the fuel flow reaches the reformation stage 116. The endothermic reformation stage requires a significant amount of heat energy to sustain the reforming operation. The fuel then flows to the fuel cell reaction stage 118, where the fuel is again heated, e.g., by the relatively hot operating environment of the converter 40. This sinusoidal like temperature profile 110 of the fuel decreases the overall operating efficiency of the converter, as well as exposes certain components (the electrolyte plate 50) to undesirable thermal stresses. The introduction of the conductive (interconnector) plate within the converter 40 "smooths" the temperature profile and creates a substantially isothermal temperature condition, in-plane and axially along the converter stack, through all stages of operation as illustrated by the isothermal profile 120.

[0077] According to one mode of operation, the internal reforming electrochemical converter catalytically reforms the hydrocarbon fuel with  $H_2O$  to produce  $H_2$  and  $CO$ , which in turn proceeds to the fuel cell portion (e.g., fuel electrode 50B) for electricity generation. It produces exhaust species  $H_2O$  and  $CO_2$ . The heat from the exothermic fuel cell reaction is conductively transferred in-plane to the conducting plates to support the endothermic reforming reaction.

[0078] According to another mode of operation, the internal reforming electrochemical converter catalytically oxidizes hydrocarbon fuel to produce  $H_2$  and  $CO$ , which proceeds to the fuel cell section for electricity generation. It produces exhaust species  $H_2O$  and  $CO_2$ . The heat from the exothermic fuel cell reaction is conductively transferred in-plane to the conductive plates 60 to support the mildly exothermic partial oxidation reforming reaction.

[0079] The internal reforming electrochemical converter can be placed in an enclosure designed for pressurized operation.

[0080] Another significant feature of the present invention is that the extended heating surfaces 72D and 72C heat the reactants delivered from the oxidizer and fuel external manifolds 47 and 48 to the operating temperature of the converter. Specifically, the extended surface 72D that protrudes into the oxidizer manifold 47 heats the oxidizer reactant, and the extended surface 72C that protrudes into the fuel manifold 48 heats the fuel reactant. The highly thermally conductive interconnector plate 60 facilitates heating of the input reactants by conductively transferring heat from the fuel cell strip to the extended surfaces or lip portions, thus heating the input reactants to the operating temperature. The extended surfaces thus function as a heat fin. This reactant heating structure provides a compact converter that is capable of being thermally integrated into a power system to realize extraordinary system efficiency.

[0081] The illustrated electrochemical converter 40 of FIGS. 3-5 is also capable of performing chemical transformation and production, while concomitantly producing electricity in a coproduction operation.

[0082] According to this embodiment, the electrochemical converter 40 is adapted to receive electricity from a power source, which initiates an electrochemical reaction within the converter and reduces selected pollutants contained within the incoming reactant into benign species. Hence, for example, the electrochemical converter 40 can be coupled to an exhaust source that contains selected pollutants, including  $NO_x$  and hydrocarbon species. The converter 40 catalytically reduces the pollutants into benign species, including  $N_2$ ,  $O_2$  and  $CO_2$ .

[0083] It will thus be seen that the invention efficiently attains the objects set forth above, among those made apparent from the preceding description. Since certain changes may be made in the above constructions without departing from the scope of the invention, it is intended that all matter contained in the above description or shown in the accompanying drawings be interpreted as illustrative and not in a limiting sense.

[0084] It is also to be understood that the following claims are to cover all generic and specific features of the invention described herein, and all statements of the scope of the invention which, as a matter of language, might be said to fall therebetween.

## Claims

1. A plate-type reformer (10) for reforming a reactant into reaction species during operation, said reformer being characterised in that it comprises a plurality of catalyst plates (14) having associated therewith one or more catalyst materials for promoting reformation and a plurality of conductive plates

- (12) formed of a thermally conducting material, said catalyst plates (14) and said conductive plates (12) being alternately stacked to form a reforming structure, the conductive plates conductively transferring heat energy in-plane to support the reforming process. 5
2. A reformer as claimed in claim 1, wherein said reforming process includes one or more reforming reactions, said reforming reactions including a catalytically assisted chemical reaction between two or more reaction species, and a catalytically assisted thermal dissociation of a single species. 10
3. A reformer as claimed in claim 1 or claim 2, wherein said reforming structure 15
- (a) includes at least one axial manifold (16) for introducing the reactant thereto and at least one manifold (20) for allowing the reaction species to exit from the reforming structure; and/or 20
- (b) has an exposed peripheral surface (13) for exchanging heat energy with an external environment. 25
4. A reformer as claimed in any one of claims 1 to 3, wherein said reforming structure includes at least one axial reactant manifold (16) for introducing the reactant thereto and peripheral exhaust means (20) for exhausting the reaction species from a peripheral portion of the reforming structure. 30
5. A reformer as claimed in any one of claims 1 to 4 further comprising 35
- a thermally conductive, gas-tight housing disposed about the stacked reforming structure to form a peripheral axial manifold (20), and optionally wherein thermally conductive, gas-tight housing includes means for exchanging heat energy with the external environment or with the reforming structure (13) and said conductive plate (12) by one of radiation, conduction and convection, and optionally 40
- means (13A) for allowing the reaction species to enter the peripheral axial manifold (20), wherein the reaction species is captured by the gas-tight housing, and 45
- optionally further comprises a gas-tight enclosure of cylindrical configuration for permitting pressurised reformer operation. 50
6. A reformer as claimed in any one of claims 1 to 5 wherein 55
- (a) the conductive plate (12) includes means (90, 92) for providing a generally isothermal condition, in plane of the conductive plate; and/or
- or
- (b) said reforming structure includes at least one axial reactant manifold (16) for introducing the reactant thereto, and wherein the conductive plates includes extension means (24) integrally formed thereon and extending into the axial reactant manifold (16) for preheating an incoming reactant; and/or
- (c) the conductive plate (12) or the catalyst plate (14) includes an in-plane surface (12A, 14A) having passage means (24) for allowing the reactant to flow over the surface of the plate, and optionally wherein said passage means (24) maintains a substantially uniform pressure drop to provide for a substantially uniform flow of reactants along an axis of the reforming structure, and further optionally wherein the reactant flow pressure drop through the passage means (24) is substantially greater than the reactant flow pressure drop within the axial manifold (16); and/or
- (d) the catalyst plate (14) or the thermally conductive plate (12) is formed of a porous catalyst material, the porous material forming passage means for allowing an incoming reactant to pass through at least a portion of the plate.
7. A reformer as claimed in any one of claims 1 to 6 wherein
- (a) the conductive plate (12) is composed of a nonmetal such as silicon carbide, or a composite material or a metal such as aluminium, copper, iron, steel alloys, nickel, nickel alloys, chromium, chromium alloys, platinum, and platinum alloys, and wherein the catalyst plate (14) is composed of a ceramic support plate having the catalyst material coating (36), platinum, nickel, nickel oxide, chromium or chromium oxide; and/or
- (b) the catalyst material (36) is selected from the group consisting of platinum, palladium, nickel, nickel oxide, iron, iron oxide, chromium, chromium oxide, cobalt, cobalt oxide, copper, copper oxide, zinc, zinc oxide, molybdenum, molybdenum oxide, and other suitable transition metals and their oxides; and/or
- (c) the reactant includes a hydrocarbon species  $O_2$ ,  $H_2O$ ,  $CO_2$ , an alkane, a hydroxyl, a hydrocarbon bonded with a carboxyl, a hydrocarbon bonded with a carbonyl, an olefin hydrocarbon, a hydrocarbon bonded with an ether, a hydrocarbon bonded with an ester, a hydrocarbon bonded with an amine, a hydrocarbon bonded with an aromatic derivative, or a hydrocarbon bonded with another organo-derivative.
8. A reformer as claimed in any one of claims 1 to 7

further including means (20) for coupling the reaction species exiting the reformer to an external fuel cell.

9. A reformer as claimed in claim 7 wherein the hydrocarbon fuel and at least one of  $H_2O$  and  $CO_2$  undergo an endothermic catalytic reformation to produce  $H_2$ ,  $CO$ ,  $H_2O$  and  $CO_2$ , the energy requirements for the endothermic reforming being supplied by energy produced by an external fuel cell, said energy being transferred from the fuel cell by the conducting plate through in-plane thermal conduction, and optionally wherein the hydrocarbon fuel and  $O_2$  undergo catalytic combustion and reformation to produce  $H_2$ ,  $CO$ ,  $H_2O$  and  $CO_2$ , and at least one of an exothermic combustion and an exothermic reaction of an external fuel cell supplementing the energy requirements for the endothermic reforming through the in-plane thermal conduction of the conducting plate (12), and wherein the  $CO$  and  $H_2O$  undergo catalytic shift reaction to form  $CO_2$  and  $H_2$ .

10. A reformer as claimed in any one of claims 1 to 9, wherein the reforming structure is cylindrical and at least one of the catalyst plate (14) and the conductive plate (12) has a diameter between about 1 inch and about 20 inches, and has a thickness between about 0.002 inch and about 0.2 inch.

11. A reformer for reforming a reactant into a reaction species during operation, said reformer being characterised in that it includes:

a plurality of porous plates (38) formed of a composite of a thermally conductive material interspersed throughout the thickness of the plates with one or more catalyst materials for promoting the reforming process, said plates (38) being stacked together to form a reforming structure (10), the plates conductively transferring heat energy in-plane of the plates to support the reforming process.

12. A reformer as claimed in claim 11 wherein said reforming structure includes

(a) at least one axial manifold (16) for introducing the reactant thereto and at least one manifold (20) for allowing the reaction species to exit from the reforming structure, and optionally peripheral exhaust means for exhausting the reaction species from a peripheral portion of the reforming structure; and/or further comprises

a thermally conductive, gas-tight housing disposed about the reforming structure to form a peripheral axial manifold (20) and configured to exchange heat with an exter-

nal environment or with the reforming structure and said reforming structure by one of radiation, conduction and convection, said gas-tight enclosure permitting pressurised reformer operation, and optionally

means for allowing the reaction species to enter the peripheral axial manifold (20), wherein the reaction species is captured by the gas-tight housing, and/or

(b) means (90, 92) for providing a generally isothermal condition through said reforming structure.

13. A reformer as claimed in claim 11 wherein said reforming structure includes at least one axial reactant manifold (16) for introducing a reactant thereto, and wherein the reforming structure includes extension means (24) integrally formed therewith and extending into the axial reactant manifold for preheating the reactant.

14. A reformer as claimed in claim 11 further including

an axial manifold (16) formed within the reforming structure, passage means (24) for allowing a reactant to flow in-plane of the reforming structure, and optionally wherein the passage means maintains a substantially uniform pressure drop to provide for a substantially uniform flow of reactants along an axis of the reforming structure, and optionally wherein said reactant flow pressure drop through the passage means (24) is substantially greater than the reactant flow pressure drop within the axial manifold (16).

15. A reformer as claimed in any one of claims 11 to 14 wherein

(a) the conductive material is composed of a nonmetal such as silicon carbide, a composite material or a metal such as aluminium, copper, iron, steel alloys, nickel, nickel alloys, chromium, chromium alloys, platinum, or platinum alloys, and optionally wherein the catalyst material is platinum, palladium, nickel, nickel oxide, iron, iron oxide, chromium, chromium oxide, cobalt, cobalt oxide, copper, copper oxide, zinc, zinc oxide, molybdenum, molybdenum oxide, or other transition metals and their oxides; and/or

(b) the reactant includes a hydrocarbon species  $O_2$ ,  $H_2O$ ,  $CO_2$ , or a hydrocarbon fuel, wherein the  $H_2O$  and  $CO_2$  undergo catalytic reformation to produce  $H_2$ ,  $CO$ ,  $H_2O$ , and  $CO_2$ , and wherein an exothermic reaction of an external fuel cell

supplements the energy requirements for the endothermic reforming reaction of the reforming structure through the thermally conductive material, and optionally

wherein the reactant includes a hydrocarbon fuel and  $O_2$  which undergo catalytic combustion and reformation to produce  $H_2$ ,  $CO$ ,  $H_2O$  and  $CO_2$ , and at least one of an exothermic combustion and an exothermic reaction of an external fuel cell supplements the energy requirements for the endothermic reforming reaction of the reforming structure through the thermally conductive material; and/or

(c) the reformer further includes means (20) for coupling the reaction species exiting the reformer to an external fuel cell.

16. A method for reforming a reactant into reaction species with a plate-type reformer (10), comprising the steps of

providing a plurality of catalyst plates (14) having associated therewith one or more catalyst materials for promoting reformation, providing a plurality of conductive plates (12) formed of a thermally conducting material, stacking said catalyst plates (14) and said conductive plates (12) to form a plate-type reforming structure (10), and conductively transferring heat energy in-plane across a surface (12A) of the conductive plate (12) to support the reforming process.

17. A method as claimed in claim 16, further comprising the step(s) of

(a) exposing a substantial portion of the peripheral surface (13) of the reforming structure for exchanging heat energy with an external environment; and/or

(b) forming a plurality of axial reactant manifolds (16) in said reforming structure for introducing the reactant thereto, and

exhausting reaction species from said peripheral portion of the reforming structure; and/or

(c) disposing a thermally conductive, gas-tight housing about the reforming structure to form a peripheral axial manifold (20) and optionally to permit pressurised reformer operation, and

allowing the reaction species to enter the peripheral axial manifold (20), wherein the reaction species is captured by the gas-tight housing; and/or

(d) forming a generally isothermal condition, in plane of the conductive plate, and optionally axially along an elongated axis of the reforming structure.

18. A method as claimed in claim 16, further comprising the steps of

(a) forming at least one axial reactant manifold (16) for introducing a reactant thereto, and

providing an integrally formed lip structure on one of an outer end and an inner end of the conductive plate (12), said lip structure extending into the axial reactant manifold (16) for preheating an incoming reactant; or

(b) forming an axial manifold (16) within the reforming structure,

forming passages (24) between the conductive plate (12) and the catalyst plate (14), and generating a reactant flow pressure drop through the passages (24) between the conductive plate (12) and the catalyst plate (14) that is substantially greater than a reactant flow pressure drop within the axial manifold (16).

19. A method as claimed in any one of claims 16 to 18, further comprising the step(s) of

(a) forming one of the thermally conductive plate (12) and the catalyst plate (14) of a porous conductive material, the porous material forming passages for allowing an incoming reactant to pass through the plate; and/or

(b) coupling the reforming structure to an external fuel cell, and

transferring heat energy produced by said fuel cell to the conductive plates through in-plane thermal conduction.

#### Patentansprüche

1. Plattenartige Reformiervorrichtung (10) zur Reformierung eines Reaktionsmittels in eine Reaktionsmittel-Abart während des Betriebes, **dadurch gekennzeichnet, daß** die Reformiervorrichtung mehrere Katalysatorplatten (14), denen ein Katalysatormaterial oder mehrere Katalysatormaterialien zugeordnet sind, um die Reformierung zu verbessern und mehrere leitfähige Platten (12) aufweist, die aus einem thermisch leitfähigen Material bestehen, wobei die Katalysatorplatten (14) und die leitfähigen Platten (12) abwechselnd gestapelt sind, um eine Reformierstruktur zu schaffen, wobei die leitfähigen Platten die Wärmeenergie in der Ebene durch Wärmeleitung übertragen, um den Reformierprozeß zu unterstützen.

2. Reformiervorrichtung nach Anspruch 1, bei welcher der Reformierprozeß eine oder mehrere Reformierreaktionen aufweist und die Reformierreaktionen eine katalytisch unterstützte chemische Reaktion zwischen zwei oder mehreren Reaktionsmittel-Abarten und eine katalytisch unterstützte thermische Dissoziation einer einzigen Abart aufweisen. 5
3. Reformiervorrichtung nach den Ansprüchen 1 oder 2, bei welcher die Reformierstruktur 10
- (a) wenigstens eine axiale Leitung (16) zur Einführung des Reaktionsmittels und wenigstens eine Leitung (20) aufweist, durch die die Reaktionsmittel-Abart aus der Reformierstruktur austreten kann; und/oder 15
- (b) eine freiliegende Umfangsoberfläche (13) aufweist, um Wärmeenergie mit einer äußeren Umgebung auszutauschen. 20
4. Reformiervorrichtung nach einem der Ansprüche 1 bis 3, bei welcher die Reformierstruktur wenigstens eine axiale Reaktionsmittelleitung (16) zur Einführung des Reaktionsmittels und eine umfängliche Auslaßleitung (20) zur Abführung der Reaktionsmittel-Abarten aus dem Umfangsabschnitt der Reformierstruktur aufweist. 25
5. Reformiervorrichtung nach einem der Ansprüche 1 bis 4, welche außerdem folgende Teile aufweist: 30
- ein thermisch leitfähiges gasdichtes Gehäuse, welches über der gestapelten Reformierstruktur angeordnet ist, um eine periphere axiale Leitung (20) zu bilden, wobei fakultativ das thermisch leitfähige gasdichte Gehäuse Mittel aufweist, um Wärmeenergie mit der äußeren Umgebung oder mit der Reformierstruktur (13) und der leitfähigen Platte (12) durch Strahlung, Wärmeleitung oder Konvektion auszutauschen und fakultativ 35
  - Mittel (13A), die die Reaktionsmittel-Abarten in die periphere axiale Leitung (20) eintreten lassen, worin die Reaktionsmittel-Abarten durch das gasdichte Gehäuse aufgefangen werden und 45
  - fakultativ weiter ein gasdichtes Behältnis zylindrischer Gestalt, um ein Reformierverfahren unter Druck zu ermöglichen. 50
6. Reformiervorrichtung nach einem der Ansprüche 1 bis 5, bei welcher 55
- (a) die leitfähige Platte (12) Mittel (90, 92) aufweist, um eine allgemein isothermische Bedingung in der Ebene der leitfähigen Platte herzustellen; und/oder
- (b) die Reformierstruktur wenigstens eine axiale Reaktionsmittelleitung (16) aufweist, um das Reaktionsmittel einzuführen und wobei die leitfähigen Platten äußere Mittel (24) aufweisen, die integral hiermit geformt sind und sich in die axiale Reaktionsmittelleitung (16) erstrecken, um das ankommende Reaktionsmittel vorzuheizen; und/oder
- (c) die leitfähige Platte (12) oder die Katalysatorplatte (14) eine in der Ebene liegende Oberfläche (12A, 14A) mit einem Kanal (24) aufweisen, damit das Reaktionsmittel über die Oberfläche der Platte strömen kann, und wobei fakultativ der Kanal (24) einen im wesentlichen gleichförmigen Druckabfall aufrechterhält, um eine im wesentlichen gleichförmige Strömung des Reaktionsmittels längs einer Achse der Reformierstruktur zu erzeugen, und wobei weiter fakultativ der Druckabfall der Reaktionsmittelströmung durch den Kanal (24) beträchtlich größer ist als der Druckabfall der Reaktionsmittelströmung innerhalb der axialen Leitung (16) und/oder
- (d) die Katalysatorplatte (14) oder die thermisch leitfähige Platte (12) aus einem porösen Katalysatomaterial besteht und das poröse Katalysatomaterial Kanäle bildet, durch welche das ankommende Reaktionsmittel durch wenigstens einen Teil der Platte hindurchströmen kann.
7. Reformiervorrichtung nach einem der Ansprüche 1 bis 6, bei welcher
- (a) die leitfähige Platte (12) aus einem nichtmetallischen Material, beispielsweise Siliziumkarbid oder einem Verbundmaterial oder einem Metall, z.B. Aluminium, Kupfer, Eisen, Stahlegierungen, Nickel, Nickellegierungen, Chrom, Chromlegierungen, Platin und Platinlegierungen besteht, und wobei die Katalysatorplatte (14) aus einer keramischen Trägerplatte zusammengesetzt ist, die einen Überzug (36) aus Katalysatomaterial besitzt, der aus Platin, Nickel, Nickeloxid, Chrom oder Chromoxid besteht; und/oder
- (b) das Katalysatomaterial (36) aus der Gruppe ausgewählt ist, die aus Platin, Paladium, Nickel, Nickeloxid, Eisen, Eisenoxid, Chrom, Chromoxid, Kobalt, Kobaltoxid, Kupfer, Kupferoxid, Zink, Zinkoxid, Molybden, Molybdenoxid und anderen geeigneten Übergangsmetallen

und ihren Oxiden besteht; und/oder

(c) das Reaktionsmittel eine Kohlenwasserstoff-Abart  $O_2$ ,  $H_2O$ ,  $CO_2$ , ein Alkan, eine Hydroxyl, einen mit einem Carboxyl verbundenen Kohlenwasserstoff, einen mit Carbonyl verbundenen Kohlenwasserstoff, einen Olifin-Kohlenwasserstoff, einen mit einem Äther verbundenen Kohlenwasserstoff, einen mit einem Ester verbundenen Kohlenwasserstoff, einen mit einem Amin verbundenen Kohlenwasserstoff, einen mit einem aromatischen Derivat verbundenen Kohlenwasserstoff oder einen Kohlenwasserstoff aufweist, der mit einem anderen organischen Derivat verbunden ist.

8. Reformiervorrichtung nach einem der Ansprüche 1 bis 7, welche außerdem Mittel (20) aufweist, um die Reaktionsmittel-Abarten, die aus der Reformiervorrichtung austreten, an eine äußere Brennstoffzelle anzukoppeln.
9. Reformiervorrichtung nach Anspruch 7, bei welcher der Kohlenwasserstoff-Brennstoff und wenigstens  $H_2O$  oder  $CO_2$  einer endothermischen katalytischen Reformierung unterworfen werden, um  $H_2$ ,  $CO$ ,  $H_2O$  und  $CO_2$  zu erzeugen, wobei der Energiebedarf für den endothermischen Reformiervorgang durch die Energie geliefert wird, die durch eine äußere Brennstoffzelle erzeugt wird, wobei die Energie von der Brennstoffzelle durch die leitfähige Platte durch Wärmeleitung zugeführt wird, und wobei fakultativ ein Kohlenwasserstoff-Brennstoff und  $O_2$  einer katalytischen Verbrennung und einer Reformierung unterworfen werden, um  $H_2$ ,  $CO$ ,  $H_2O$  und  $CO_2$  zu erzeugen, und wobei wenigstens eine exothermische Verbrennung oder eine exothermische Reaktion einer äußeren Brennstoffzelle den Energiebedarf für die endothermische Reformierung durch die Wärmeleitung in der Ebene der leitfähigen Platte (12) deckt, und wobei  $CO$  und  $H_2O$  einer katalytischen Wechselreaktion ausgesetzt werden, um  $CO_2$  und  $H_2$  zu erzeugen.
10. Reformiervorrichtung nach einem der Ansprüche 1 bis 9, bei welcher die Reformierstruktur zylindrisch ist und wenigstens eine der zylindrischen Platte (14) und der leitfähigen Platte (12) einen Durchmesser zwischen etwa 1 Zoll und etwa 20 Zoll und eine Dicke zwischen etwa 0,002 Zoll und etwa 0,2 Zoll aufweist.
11. Reformiervorrichtung zur Reformierung eines Reaktionsmittels in eine Reaktionsmittel-Abart während des Betriebs, wobei die Reformiervorrichtung dadurch gekennzeichnet ist, daß sie mehrere poröse Platten (38) aufweist, die aus einem thermisch leitfähigen Material bestehen, das

über die Dicke der Platten mit wenigstens einem Katalysatomaterial durchsetzt ist, um den Reformiervorgang zu verbessern, wobei die Platten (38) gestapelt sind, um eine Reformierstruktur (10) zu schaffen, bei der die Platten durch Wärmeleitung Wärmeenergie in der Ebene der Platten übertragen, um den Reformiervorgang zu unterstützen.

12. Reformiervorrichtung nach Anspruch 11, bei welcher die Reformierstruktur folgende Teile umfaßt:

(a) wenigstens eine axiale Leitung (16) zum Einführen des Reaktionsmittels und wenigstens eine Leitung (20), durch die die Reaktionsmittel-Abarten aus der Reformierstruktur austreten können und fakultativ periphere Austrittsmittel, um die Reaktionsmittel-Abarten aus einem Umfangsteil der Reformierstruktur austreten zu lassen; und/oder

ein thermisch leitfähiges gasdichtes Gehäuse, welches um die Reformierstruktur herum angeordnet ist, um eine periphere axiale Leitung (20) zu schaffen, die derart angeordnet und ausgebildet ist, daß Wärme mit der äußeren Umgebung oder mit der Reformierstruktur durch Strahlung, Wärmeleitung oder Konvektion ausgetauscht wird, wobei das gasdichte Gehäuse eine Druckreformier-Operation ermöglicht, und fakultativ

Mittel, die die Reaktionsmittel-Abarten in die periphere axiale Leitung (20) eintreten lassen, wobei die Reaktionsmittel-Abarten durch das gasdichte Gehäuse aufgefangen werden, und/oder

(b) Mittel (90, 92), um eine allgemein isothermische Bedingung durch die Reformierstruktur herzustellen.

13. Reformiervorrichtung nach Anspruch 11, bei welcher die Reformierstruktur wenigstens eine axiale Reaktionsmittelleitung (16) aufweist, um ein Reaktionsmittel zuzuführen, und wobei die Reformierstruktur einen Fortsatz (24) aufweist, der integral hiermit hergestellt ist und sich in die axiale Reaktionsmittelleitung hinein erstreckt, um das Reaktionsmittel vorzuheizen.

14. Reformiervorrichtung nach Anspruch 11, welche außerdem folgende Mittel aufweist:

eine axiale Leitung (16), die in der Reformierstruktur ausgebildet ist,

Kanalmittel (24), durch die ein Reaktionsmittel

in der Ebene der Reformierstruktur strömen kann und wobei fakultativ die Kanalmittel einen im wesentlichen gleichförmigen Druckabfall aufrechterhalten, um eine im wesentlichen gleichförmige Strömung von Reaktionsmittel längs einer Achse der Reformierstruktur zu schaffen, wobei fakultativ der Druckabfall der Reaktionsmittelströmung durch die Kanalmittel (24) beträchtlich größer ist als der Druckabfall der Reaktionsmittelströmung innerhalb der axialen Leitung (16).

15. Reformiervorrichtung nach einem der Ansprüche 11 bis 14, bei welcher

(a) das leitfähige Material aus einem Nicht-Metall, beispielsweise Siliziumkarbid, einem Verbundmaterial oder einem Metall besteht, beispielsweise aus Aluminium, Kupfer, Eisen, Stahllegierungen, Nickel, Nickellegierungen, Chrom, Chromlegierungen, Platin oder Platinlegierungen und wobei fakultativ das Katalysatormaterial Platin, Paladium, Nickel, Nickeloxid, Eisen, Eisenoxid, Chrom, Chromoxid, Kobalt, Kobaltoxid, Kupfer, Kupferoxid, Zink, Zinkoxid, Molybden, Molybdenoxid oder ein anderes Übergangsmetall und andere Oxide sind; und/oder wobei

(b) das Reaktionsmittel eine Kohlenwasserstoff-Abart  $O_2$ ,  $H_2O$ ,  $CO_2$  oder einen Kohlenwasserstoff-Brennstoff aufweist, wobei  $H_2O$  und  $CO_2$  einer katalytischen Reformierung unterworfen werden, um  $H_2$ ,  $CO$ ,  $H_2O$  und  $CO_2$  zu erzeugen, und wobei eine exothermische Reaktion einer äußeren Brennstoffzelle den Energiebedarf für die endothermische Reformierungsreaktion der Reformierstruktur über das thermisch leitfähige Material deckt, und wobei fakultativ

das Reaktionsmittel einen Kohlenwasserstoff-Brennstoff und  $O_2$  aufweist, die einer katalytischen Verbrennung und einer Reformierung unterworfen werden, um  $H_2$ ,  $CO$ ,  $H_2O$  und  $CO_2$  zu erzeugen, und wobei wenigstens eine exothermische Verbrennung oder eine exothermische Reaktion einer äußeren Brennstoffzelle den Energiebedarf für die endothermische Reformierungsreaktion der Reformierstruktur über das thermisch leitfähige Material deckt; und/oder

(c) die Reformiervorrichtung außerdem Mittel (20) aufweist, um die Reaktionsmittel-Abarten, die aus der Reformiervorrichtung austreten, an eine äußere Brennstoffzelle anzukoppeln.

16. Verfahren zur Reformierung eines Reaktionsmittels

in einer Reaktionsmittel-Abart mittels einer plattenartigen Reformiervorrichtung (10), welches die folgenden Schritte aufweist:

es werden mehrere Katalysatorplatten (14) vorgesehen, denen jeweils ein Katalytmaterial oder mehrere Katalytmaterialien zugeordnet sind, um die Reformierung zu verbessern; es werden mehrere leitfähige Platten (12) vorgesehen, die ein thermisch leitfähiges Material bilden; es werden die Katalysatorplatten (14) und die leitfähigen Platten (12) gestapelt, um die plattenartige Reformierstruktur (10) zu schaffen, und es wird durch Wärmeleitung Wärmeenergie in der Ebene über eine Oberfläche (12A) der leitfähigen Platte (12) übertragen, um das Reformierverfahren zu unterstützen.

17. Verfahren nach Anspruch 16, welches weiter die folgenden Schritte umfaßt:

(a) es wird ein beträchtlicher Teil der Umfangsoberfläche (13) der Reformierstruktur zum Austausch der Wärmeenergie einer äußeren Umgebung ausgesetzt; und/oder

(b) es werden mehrere axiale Reaktionsmittelleitungen (16) in der Reformierstruktur geschaffen, um das Reaktionsmittel zuzuführen, und

es werden Reaktionsmittel-Abarten aus dem Umfangsabschnitt der Reformierstruktur abgeführt, und/oder

(c) es wird ein thermisch leitfähiges gasdichtes Gehäuse um die Reformierstruktur herum angeordnet, um eine periphere axiale Leitung (20) zu bilden und fakultativ um eine Druckreformier-Arbeitsweise zuzulassen, und

man läßt die Reaktionsmittel-Abarten in die periphere axiale Leitung (20) eintreten, worin die Reaktionsmittel-Abarten durch das gasdichte Gehäuse aufgefangen werden; und/oder

(d) es wird eine allgemein isothermische Bedingung in der Ebene der leitfähigen Platte und fakultativ axial längs einer langgestreckten Achse der Reformierstruktur geschaffen.

18. Verfahren nach Anspruch 16, welches weiter die folgenden Schritte umfaßt:

(a) es wird wenigstens eine axiale Reaktionsmittelleitung (16) gebildet, um ein Reaktionsmittel einzuführen, und



es wird eine integral geformte Lippenstruktur auf einem äußeren Ende oder einem inneren Ende der leitfähigen Platte (12) gebildet, wobei sich die Lippenstruktur in die axiale Reaktionsmittelleitung (16) hinein erstreckt, um ein einströmendes Reaktionsmittel vorzuheizen; oder

(b) es wird eine axiale Leitung (16) innerhalb der Reformierstruktur geschaffen;

es werden Kanäle (24) zwischen der leitfähigen Platte (12) und der Katalysatorplatte (14) ausgebildet, und

es wird ein Druckabfall einer Reaktionsmittelströmung durch die Kanäle (24) zwischen der leitfähigen Platte (12) und der Katalysatorplatte (14) erzeugt, wobei dieser Druckabfall beträchtlich größer ist als der Druckabfall einer Reaktionsmittelströmung innerhalb der axialen Leitung (16).

19. Verfahren nach einem der Ansprüche 16 bis 18, welches weiter die folgenden Schritte umfaßt:

(a) es wird die thermisch leitfähige Platte (12) oder die Katalysatorplatte (14) aus einem porösen, leitfähigen Material hergestellt, wobei das poröse Material Kanäle bildet, die es einem einströmenden Reaktionsmittel ermöglichen, durch die Platte hindurchzuströmen; und/oder

(b) es wird die Reformierstruktur an einer äußeren Brennstoffzelle angekoppelt, und es wird Wärmeenergie, die durch die Brennstoffzelle erzeugt wird, auf die leitfähigen Platten über Wärmeleitung in der Ebene der Platte übertragen.

## Revendications

1. Reformeur (10) du type à plaques pour le reformage d'un réactif en une espèce réactionnelle au cours de la mise en service, ledit reformeur étant caractérisé en ce qu'il comprend plusieurs plaques de catalyseurs (14) auxquelles sont associées une ou plusieurs matières de catalyseurs pour favoriser le reformage et plusieurs plaques conductrices (12) réalisées en une matière manifestant une conduction thermique, lesdites plaques de catalyseurs (14) et lesdites plaques conductrices (12) étant empilées en alternance pour former une structure de reformage, les plaques conductrices transférant de l'énergie thermique par conduction en plan pour supporter le processus de reformage.

2. Reformeur selon la revendication 1, dans lequel ledit processus de reformage englobe une ou plusieurs réactions de reformage, lesdites réactions de reformage englobant une réaction chimique assistée par catalyseur entre deux ou plusieurs espèces réactionnelles, et une dissociation thermique d'une espèce unique assistée par catalyseur.

3. Reformeur selon la revendication 1 ou 2, dans lequel ladite structure de reformage

(a) englobe au moins un collecteur axial (16) pour l'introduction du réactif et au moins un collecteur (20) pour permettre à l'espèce réactionnelle de quitter la structure de reformage; et/ou (b) possède une surface périphérique exposée (13) pour échanger de l'énergie thermique avec l'environnement externe.

4. Reformeur selon l'une quelconque des revendications 1 à 3, dans lequel ladite structure de reformage englobe au moins un collecteur de réactif axial (16) pour l'introduction du réactif et un moyen d'évacuation périphérique (20) pour l'évacuation de l'espèce réactionnelle d'une portion périphérique de la structure de reformage.

5. Reformeur selon l'une quelconque des revendications 1 à 4, comprenant en outre

un boîtier à conduction thermique étanche aux gaz disposé autour de la structure de reformage empilée pour former un collecteur axial périphérique (20), et le cas échéant dans lequel le boîtier à conduction thermique étanche aux gaz englobe un moyen pour échanger de l'énergie thermique avec l'environnement externe ou avec la structure de reformage (13) et avec lesdites plaques conductrices (12) soit par rayonnement, soit par conduction, soit par convection, et le cas échéant un moyen (13) pour permettre à l'espèce réactionnelle de pénétrer dans le collecteur axial périphérique (20), dans lequel l'espèce réactionnelle est capturée par le boîtier étanche aux gaz, et comprend en outre le cas échéant une enceinte étanche aux gaz de configuration cylindrique pour permettre une mise en service du reformeur sous pression.

6. Reformeur selon l'une quelconque des revendications 1 à 5, dans lequel

(a) les plaques conductrices (12) englobent des moyens (90, 92) pour procurer une condition généralement isothermique dans le plan des plaques conductrices; et/ou

(b) ladite structure de reformage englobe au moins un collecteur de réactif axial (16) pour l'introduction du réactif, et dans lequel les plaques conductrices englobent des moyens de prolongement (24) faisant partie intégrante des premières citées et s'étendant dans le collecteur de réactif axial (16) pour préchauffer un réactif entrant ; et/ou

(c) les plaques conductrices (12) ou les plaques de catalyseurs (14) englobent une surface plane (12A, 14A) comportant des moyens de passage (24) pour permettre au réactif de s'écouler par-dessus la surface des plaques, et le cas échéant dans lequel lesdits moyens de passage (24) maintiennent une chute de pression essentiellement uniforme pour procurer un écoulement de réactif essentiellement uniforme le long de l'axe de la structure de reformage, et dans lequel en outre le cas échéant la chute de pression de l'écoulement du réactif à travers le moyen de passage (24) est essentiellement supérieure à la chute de pression de l'écoulement du réactif à l'intérieur du collecteur axial (16); et/ou

(d) les plaques de catalyseurs (14) ou les plaques (12) à conduction thermique sont réalisées en une matière catalytique poreuse, la matière poreuse formant des moyens de passage pour permettre à un réactif entrant de passer à travers au moins une portion des plaques.

7. Reformeur selon l'une quelconque des revendications 1 à 6, dans lequel

(a) les plaques conductrices (12) sont composées d'un non-métal tel que du carbure de silicium, ou d'une matière composite ou d'un métal tel que l'aluminium, le cuivre, le fer, des alliages à base d'acier, le nickel, des alliages à base de nickel, le chrome, des alliages à base de chrome, le platine et des alliages à base de platine, et dans lequel les plaques de catalyseurs (14) sont composées de plaques de support en céramique comportant, à titre de revêtement (36) constitué d'une matière catalytique, du platine, du nickel, de l'oxyde de nickel, du chrome ou de l'oxyde de chrome; et/ou

(b) la matière catalytique (36) est choisie parmi le groupe constitué par le platine, le palladium, le nickel, l'oxyde de nickel, le fer, l'oxyde de fer, le chrome, l'oxyde de chrome, le cobalt, l'oxyde de cobalt, le cuivre, l'oxyde de cuivre, le zinc, l'oxyde de zinc, le molybdène, l'oxyde de molybdène, et d'autres métaux transitoires appropriés ainsi que leurs oxydes; et/ou

(c) le réactif englobe une espèce d'hydrocarbure, O<sub>2</sub>, H<sub>2</sub>O, CO<sub>2</sub>, un alcane, un hydroxyle, un hydrocarbure lié à un carboxyle, un hydrocar-

bure lié à un carbonyle, un hydrocarbure oléfinique, un hydrocarbure lié à un éther, un hydrocarbure lié à un ester, un hydrocarbure lié à une amine, un hydrocarbure lié à un dérivé aromatique ou un hydrocarbure lié à un autre dérivé organique.

8. Reformeur selon l'une quelconque des revendications 1 à 7, englobant en outre des moyens 20 pour coupler l'espèce réactionnelle quittant le reformeur à une cellule combustible externe.

9. Reformeur selon la revendication 7, dans lequel le carburant d'hydrocarbure et au moins un élément choisi parmi le groupe comprenant du H<sub>2</sub>O et du CO<sub>2</sub> subissent un reformage catalytique endothermique pour produire du H<sub>2</sub>, du CO, du H<sub>2</sub>O et du CO<sub>2</sub>, les exigences énergétiques pour le reformage endothermique étant satisfaites par l'énergie produite par une cellule combustible externe, ladite énergie étant transférée à partir de la cellule combustible par les plaques conductrices via une conduction thermique en plan, et le cas échéant dans lequel le carburant d'hydrocarbure et le O<sub>2</sub> subissent une combustion catalytique et un reformage pour produire du H<sub>2</sub>, du CO, du H<sub>2</sub>O et du CO<sub>2</sub>, et sont soumis à au moins une réaction choisie parmi le groupe comprenant une combustion exothermique et une réaction exothermique d'une cellule combustible externe satisfaisant aux exigences énergétique pour le reformage endothermique via la conduction thermique des plaques conductrices (12) en plan, et dans lequel le CO et le H<sub>2</sub>O subissent une réaction de déplacement catalytique pour former du CO<sub>2</sub> et du H<sub>2</sub>.

10. Reformeur selon l'une quelconque des revendications 1 à 9, dans lequel la structure de reformage est de forme cylindrique et au moins un des éléments choisi parmi le groupe comprenant les plaques de catalyseurs (14) et les plaques conductrices (12) possède un diamètre entre environ 1 pouce et environ 20 pouces, et possède une épaisseur entre environ 0,002 pouce et environ 0,2 pouce.

11. Reformeur pour reformer un réactif en une espèce réactionnelle lors de la mise en service, ledit reformeur étant **caractérisé en ce qu'il englobe :**

plusieurs plaques poreuses (38) formées à l'aide d'un composite d'une matière à conduction thermique parsemées, sur l'épaisseur des plaques, avec une ou plusieurs matières catalytiques pour favoriser le processus de reformage, lesdites plaques (38) étant empilées l'une sur l'autre pour former une structure de reformage (10), les plaques transférant de l'énergie thermique par conduction dans le plan des plaques pour supporter le processus de reformage.

**12. Reformeur selon la revendication 11, dans lequel ladite structure de reformage englobe**

(a) au moins un collecteur de réactif axial (16) pour l'introduction du réactif et au moins un collecteur (20) pour permettre à l'espèce réactionnelle de quitter la structure de reformage, et le cas échéant un moyen d'évacuation périphérique pour l'évacuation de l'espèce réactionnelle d'une portion périphérique de la structure de reformage; et/ou comprend en outre

un boîtier à conduction thermique étanche aux gaz disposé autour de la structure de reformage pour former un collecteur axial périphérique (20) et configuré pour échanger de l'énergie thermique avec l'environnement externe ou avec la structure de reformage et avec ladite structure de reformage soit par rayonnement, soit par conduction, soit par convection, ladite enceinte étanche aux gaz permettant une mise en service du reformeur sous pression, et le cas échéant

un moyen pour permettre à l'espèce réactionnelle de pénétrer dans le collecteur axial périphérique, dans lequel l'espèce réactionnelle est capturée par le boîtier étanche aux gaz, et/ou

(b) des moyens (90, 92) pour procurer une condition généralement isothermique à travers ladite structure de reformage.

**13. Reformeur selon la revendication 11, dans lequel ladite structure de reformage englobe au moins un collecteur de réactif axial (16) pour l'introduction d'un réactif, et dans lequel la structure de reformage englobe des moyens de prolongement (24) faisant partie intégrante de la première citée et s'étendant dans le collecteur de réactif axial pour préchauffer le réactif.**

**14. Reformeur selon la revendication 11, englobant en outre**

un collecteur axial (16) formé à l'intérieur de la structure de reformage, des moyens de passage (24) pour permettre à un réactif de s'écouler dans le plan de la structure de reformage, et le cas échéant dans lequel des moyens de passage (24) maintiennent une chute de pression essentiellement uniforme pour procurer un écoulement de réactif essentiellement uniforme le long de l'axe de la structure de reformage, et dans lequel en outre le cas échéant la chute de pression de l'écoulement du réactif à travers le moyen de passa-

ge (24) est essentiellement supérieure à la chute de pression de l'écoulement du réactif à l'intérieur du collecteur axial (16).

**15. Reformeur selon l'une quelconque revendication 11 à 14, dans lequel**

(a) la matière conductrice est composée d'un non-métal tel que du carbure de silicium, d'une matière composite ou d'un métal tel que l'aluminium, le cuivre, le fer, des alliages à base d'acier, le nickel, des alliages à base de nickel, le chrome, des alliages à base de chrome, le platine et des alliages à base de platine, et le cas échéant dans lequel la matière catalytique est le platine, le palladium, le nickel, l'oxyde de nickel, le fer, l'oxyde de fer, le chrome, l'oxyde de chrome, le cobalt, l'oxyde de cobalt, le cuivre, l'oxyde de cuivre, le zinc, l'oxyde de zinc, le molybdène, l'oxyde de molybdène, ou d'autres métaux transitoires appropriés, ainsi que leurs oxydes; et/ou

(b) le réactif englobe une espèce d'hydrocarbure,  $O_2$ ,  $H_2O$ ,  $CO_2$ , ou un carburant d'hydrocarbure, dans lequel le  $H_2O$  et le  $CO_2$  subissent un reformage catalytique pour produire du  $H_2$ , du  $CO$ , du  $H_2O$  et du  $CO_2$ , et dans lequel une réaction endothermique d'une cellule combustible externe satisfait aux exigences énergétiques pour la réaction de reformage endothermique de la structure de reformage via la matière à conduction thermique, et le cas échéant dans lequel le réactif englobe un carburant d'hydrocarbure et du  $O_2$  qui subissent une combustion catalytique et un reformage pour produire du  $H_2$ , du  $CO$ , du  $H_2O$  et du  $CO_2$ , et sont soumis à au moins une réaction choisie parmi le groupe comprenant une combustion exothermique et une réaction exothermique d'une cellule combustible externe satisfaisant aux exigences énergétiques pour la réaction de reformage endothermique via la matière à conduction thermique; et/ou

(c) le reformeur englobe en outre des moyens (20) pour coupler l'espèce réactionnelle quittant le reformeur à une cellule combustible externe.

**16. Procédé pour le reformage d'un réactif en une espèce réactionnelle avec un reformeur (10) du type à plaques, comprenant les étapes consistant à**

procurer plusieurs plaques de catalyseurs (14) auxquelles sont associées une ou plusieurs matières catalytiques pour favoriser le reformage, procurer plusieurs plaques conductrices (12) réalisées à partir d'une matière à conduction

thermique,  
empiler lesdites plaques de catalyseurs 14 et  
lesdites plaques conductrices 12 pour former  
une structure de reformage (10) du type à pla-  
ques, et  
transférer par conduction de l'énergie thermi-  
que en plan à travers une surface (12A) des  
plaques conductrices (12) pour supporter le  
processus de reformage.

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17. Procédé selon la revendication 16, comprenant en  
outre l'étape ou les étapes consistant à

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(a) exposer une portion substantielle de la sur-  
face périphérique (13) de la structure de refor-  
mage pour échanger de l'énergie thermique  
avec un environnement externe; et/ou

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(b) former plusieurs collecteurs de réactif  
axiaux (16) dans ladite structure de reformage  
pour l'introduction du réactif et pour l'évacua-  
tion de l'espèce réactionnelle de ladite portion  
périphérique de la structure de reformage; et/  
ou

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(c) disposer un boîtier à conduction thermique  
étanche aux gaz autour de la structure de re-  
formage pour former un collecteur axial péri-  
phérique (20) et le cas échéant pour permettre  
une mise en service du reformeur sous pres-  
sion, et pour permettre à l'espèce réactionnelle  
de pénétrer dans le collecteur excellent péri-  
phérique (20) dans lequel l'espèce réactionnel-  
le est capturée par le boîtier étanche aux gaz;  
et/ou

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(d) former une condition généralement isother-  
mique dans le plan des plaques conductrices  
et le cas échéant en direction axiale le long de  
l'axe longitudinal de la structure de reformage.

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18. Procédé selon la revendication 16, comprenant en  
outre les étapes consistant à

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(a) former au moins un collecteur de réactif  
axial (16) pour l'introduction d'un réactif, et  
procurer une structure de lèvre faisant  
partie intégrante des plaques conductrices  
(12), soit sur l'extrémité externe, soit sur l'ex-  
trémité interne de ces dernières, ladite structu-  
re de lèvre s'étendant dans le collecteur de  
réactif axial (16) pour préchauffer un réactif en-  
trant; ou

45

50

(b) former un collecteur axial (16) à l'intérieur  
de la structure de reformage,

former des passages (24) entre les pla-  
ques conductrices (12) et les plaques de

55

catalyseurs (14), et  
générer une chute de pression de l'écoule-  
ment de réactif à travers les passages (24)

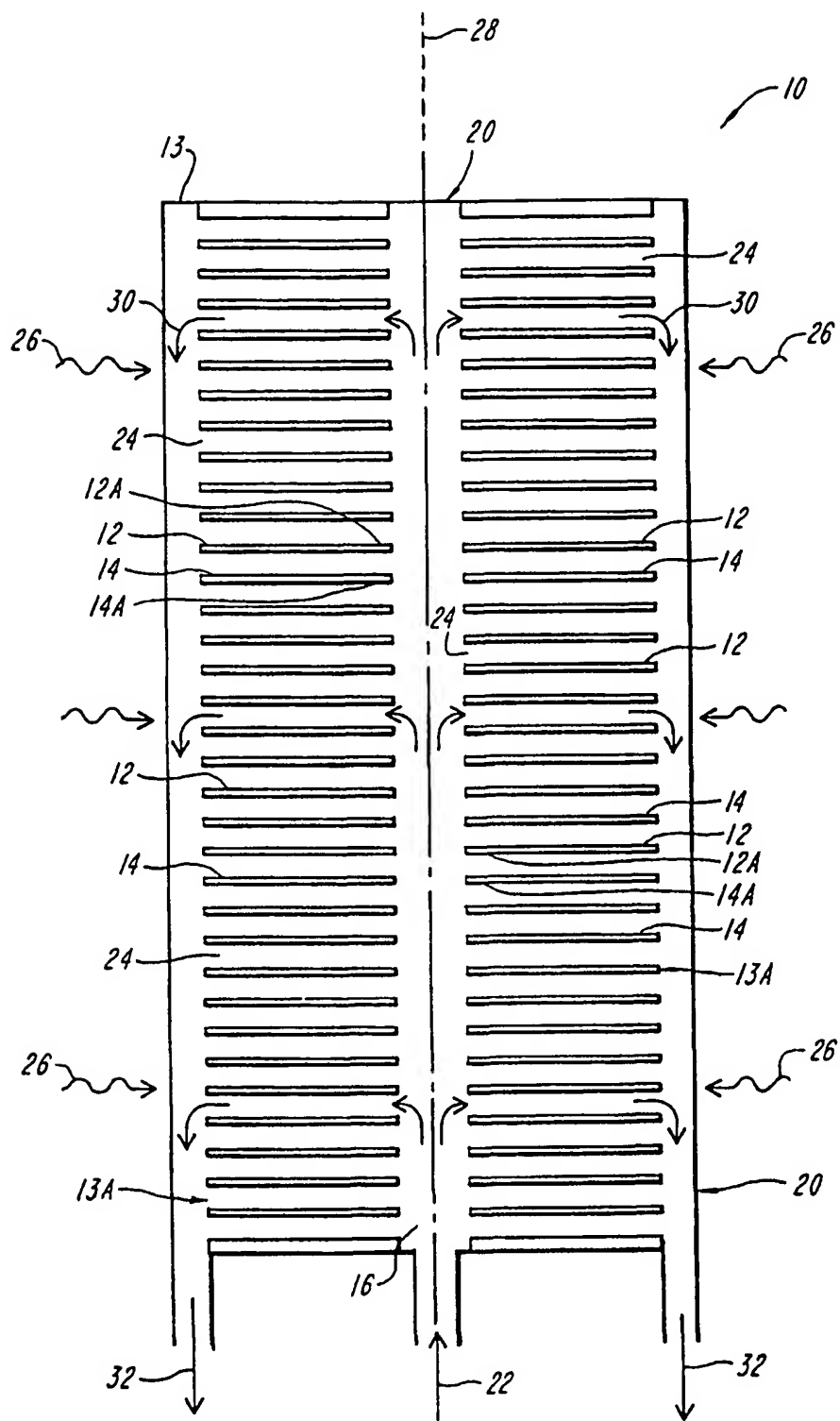
entre les plaques conductrices (12) et les  
plaques de catalyseurs (14), qui est essen-  
tiellement supérieure à la chute de pres-  
sion de l'écoulement de réactif à l'intérieur  
du collecteur axial (16).

19. Procédé selon l'une quelconque des revendications  
16 à 18, comprenant en outre l'étape ou les étapes  
consistant à

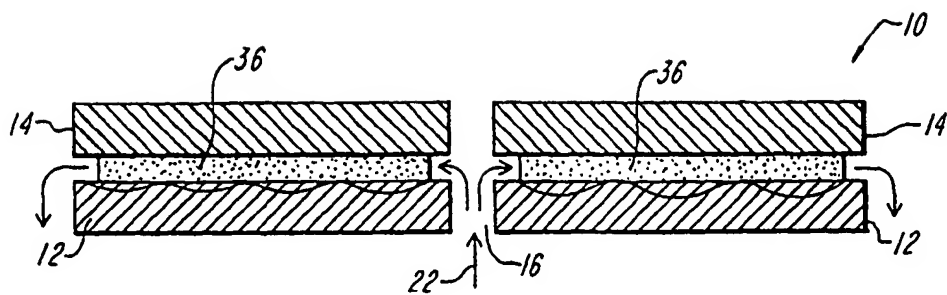
(a) former, soit les plaques à conduction ther-  
mique (12), soit les plaques de catalyseurs (14)  
en une matière conductrice poreuse, la matière  
poreuse formant des passages pour permettre  
à un réactif entrant de passer à travers les pla-  
ques; et/ou

(b) coupler la structure de reformage à une cel-  
lule combustible externe, et

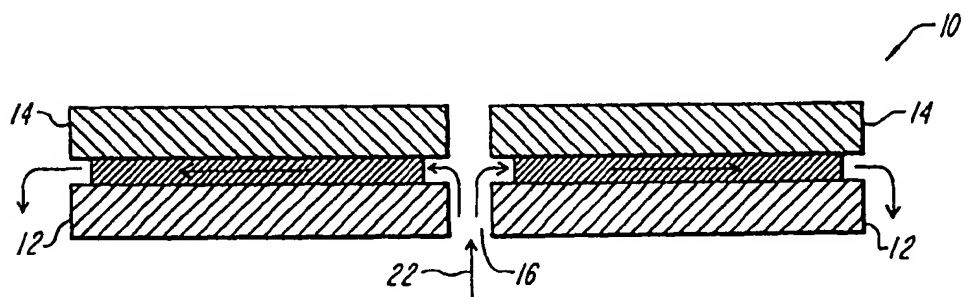
transférer de l'énergie thermique produite  
par ladite cellule combustible aux plaques con-  
ductrices via une conduction thermique en  
plan.



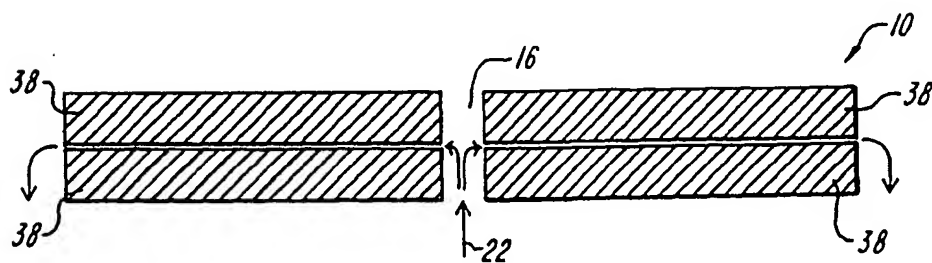
**FIG. 1**



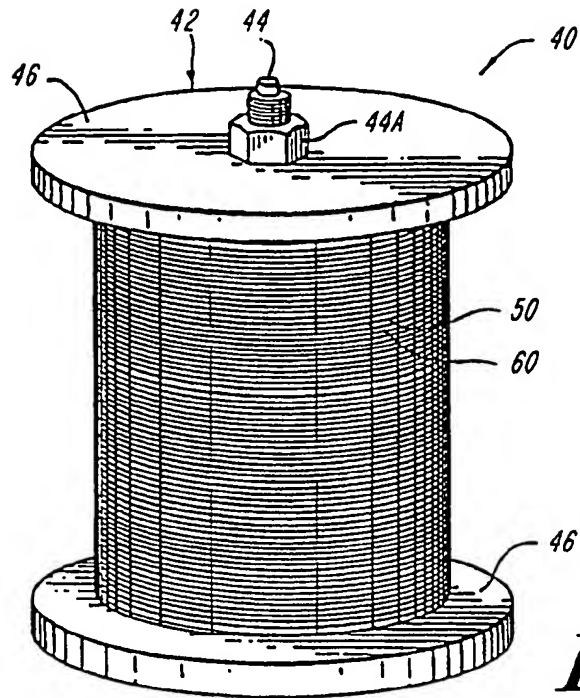
**FIG. 2A**



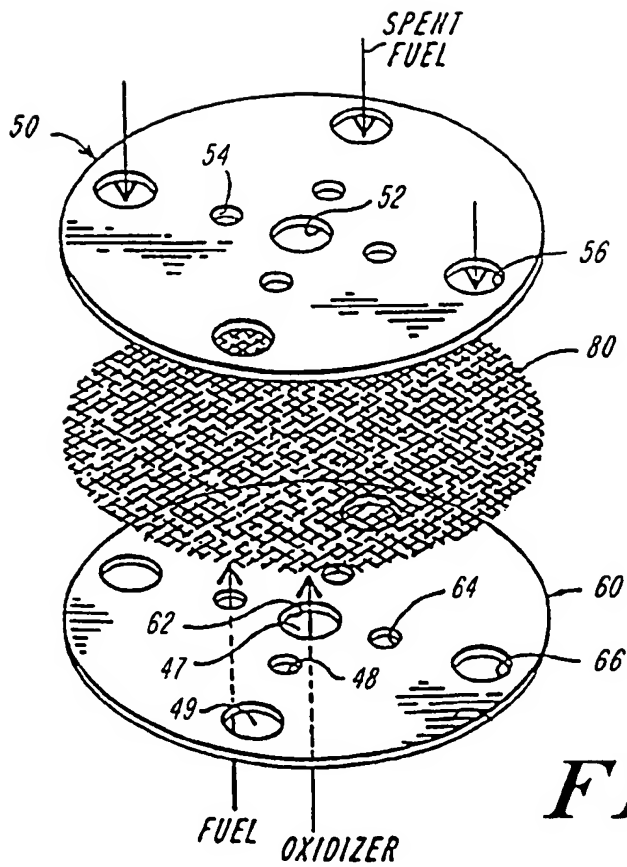
**FIG. 2B**



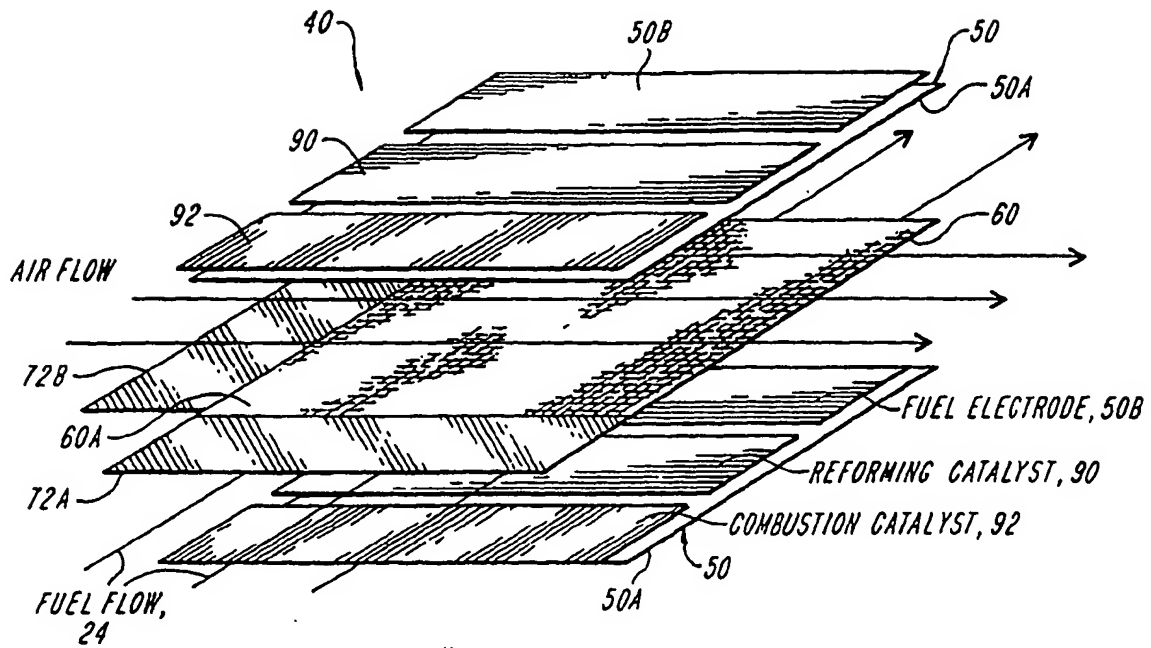
**FIG. 2C**



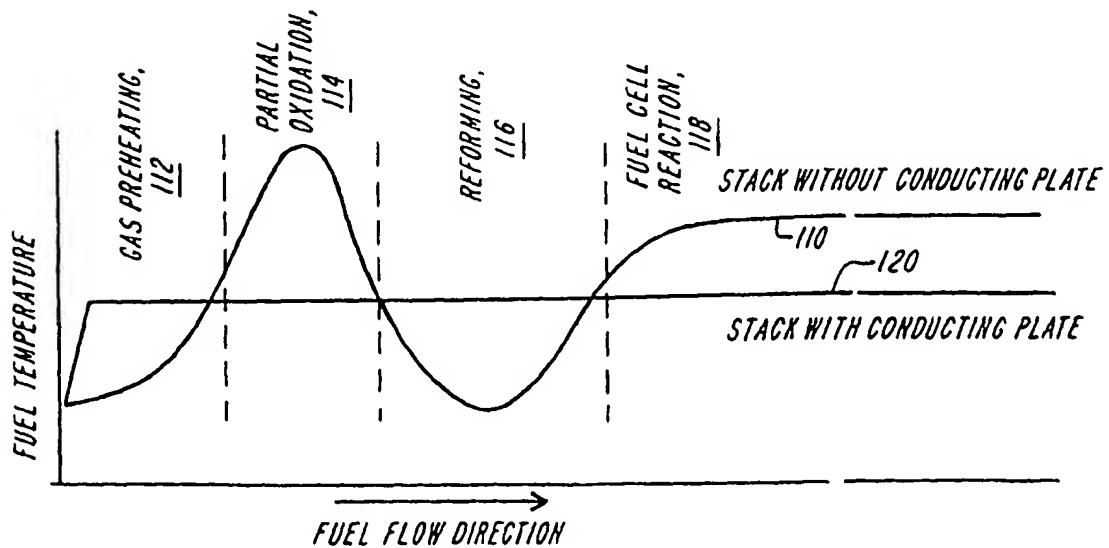
**FIG. 3**



**FIG. 4**



**FIG. 5**



**FIG. 6**